

Problem 1.

$$\alpha = -4np - m^{-1}$$

$$\gamma^2 = (\alpha + j\beta)^2 = j\omega\mu(\sigma + j\omega\varepsilon)$$

$$(\alpha^2 - \beta^2) + j(2\alpha\beta) = -\omega^2\mu\varepsilon + j\omega\mu\sigma = -\omega^2\mu_0(18.5\varepsilon_0) + j\omega\mu_0\sigma$$

$$(\alpha^2 - \beta^2) = -\omega^2\mu_0(18.5\varepsilon_0)$$

$$\Rightarrow \beta = \sqrt{\alpha^2 + 18.5\omega^2\mu_0\varepsilon_0} \approx 9.86 \text{ rad} - m^{-1}$$

$$\text{and } 2\alpha\beta = \omega\mu_0\sigma \Rightarrow \sigma = \frac{2\alpha\beta}{\omega\mu_0} \approx 0.1 \text{ Sm}^{-1}$$

Problem 1. Cont.

$$\eta_c = |\eta_c| e^{j\phi_n} = 74.2 e^{j0.386}$$

$$\text{So } \mathcal{E}_x(z, t) = 2e^{-4z} \cos(\omega t - 9.86z) V - m^{-1}$$

$$\mathcal{H}_y(z, t) = 2.7 \times 10^{-2} \cos(\omega t - 9.86z - 0.386) A - m^{-1}$$

$$S_{av} = \hat{z} \left(2.7 \times 10^{-2} \right) e^{-bz} \cos(0.386) \approx \hat{z} \left(2.5 \times 10^{-2} e^{-8z} \right) W - m^{-2}$$

$$\begin{aligned} P_{entering} &= (\text{Area of } xy \text{ plane}) |S_{av}(z=0)| \\ &= (ab) \left(2.5 \times 10^{-2} \right) = 1.25 \times 10^{-2} W \end{aligned}$$

$$\begin{aligned} P_{exiting} &= (\text{Area on } z = d \text{ plane}) |S_{av}(z=d)| \\ &= (ab) \left(2.5 \times 10^{-2} \right) \left(e^{-8} \right) = 4.19 \times 10^{-6} W \end{aligned}$$

Problem 1. Cont.

$$P_d = \bar{\mathbf{j}} \cdot \bar{\mathbf{E}} = \sigma \bar{\mathbf{E}} \cdot \bar{\mathbf{E}} = \sigma |Ec|^2 = 0.4e^{-8z} \cos^2(\omega t - 9.86z) \\ = 0.2e^{-8z} + 0.2e^{-8z} \cos[2(\omega t - 9.86z)]$$

$$\Rightarrow [P_d]_{av} = 0.2e^{-8z} \text{ W} \cdot \text{m}^{-3}$$

$$P_{total} = \int_V [P_d]_{av} dV = \int_0^1 (ab) 0.2e^{-8z} dz = \int_0^1 (.5) 0.2e^{-8z} dz \approx 1.25 \times 10^{-2} \text{ W}$$

Note that $P_{total} = P_{entering} - P_{exiting}$

Problem 2.

Note that since for normal incidence, $1 + \Gamma = \tau$, the reflection and transmission coefficients must be $\Gamma = -0.5$ and $\tau = 0.5$ respectively. For loss-less nonmagnetic case, the reflection and transmission coefficients can be simplified as

$$\Gamma = \frac{\sqrt{\epsilon_{1r}} - \sqrt{\epsilon_{2r}}}{\sqrt{\epsilon_{1r}} + \sqrt{\epsilon_{2r}}} = -0.5$$

$$\tau = \frac{2\sqrt{\epsilon_{1r}}}{\sqrt{\epsilon_{1r}} + \sqrt{\epsilon_{2r}}} = 0.5$$

dividing these two equations with one another yields

$$0.5 - 0.5 \frac{\sqrt{\epsilon_{2r}}}{\sqrt{\epsilon_{1r}}} = -1 \Rightarrow \frac{\epsilon_{2r}}{\epsilon_{1r}} = 9$$

Problem 3.

At 3GHz, the skin depth of copper is $\delta \approx 1.15 \mu\text{m}$ which means that we can easily reflect multiple reflections for a copper foil of $10 \mu\text{m}$ thickness. The reflection coefficient at air-copper interface is given

$$\Gamma = \frac{\eta_c - \eta_0}{\eta_c + \eta_0} \quad (\eta_c \text{ is the intrinsic impedance of copper})$$

where

$$\eta_c = \sqrt{\frac{j\omega\mu_0}{\sigma}} = \sqrt{\frac{\omega\mu_0}{\sigma}} e^{j45^\circ} = \frac{2\pi\sqrt{f}}{\sqrt{5.8}} (1 + j)$$

$$\eta_c \approx 2.61 \times 10^{-7} \sqrt{f} (1 + j) \Omega$$

$$\Gamma = \frac{\eta_c - \eta_0}{\eta_c + \eta_0} = \frac{2.61 \times 10^{-7} \sqrt{f} (1 + j) \Omega - 377 \Omega}{2.61 \times 10^{-7} \sqrt{f} (1 + j) \Omega + 377 \Omega}$$

Problem 3. Cont.

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Problem 3. Cont.

At 3GHz

$$\Gamma \cong 0.9993623e^{j179.997^\circ}$$

$$(S_{av})_r = |\Gamma^2|(S_{av})_i = 998.72W - m^{-2}$$

$$(S_{av})_t = (1 - |\Gamma^2|)(S_{av})_i = 1.274993W - m^{-2}$$

for copper with $\sigma = 5.78 \times 10^7 S - m^{-1}$, at 3GHz, we have

$$\alpha \approx 827593.621 \text{ np} - m^{-1}$$

$$(S_{av})_{emerging} = [(S_{av})_t (e^{-2\alpha z})]_{z=10\mu m} \approx 82.626nW - m^{-2}$$

Thus 10um sheet of copper is extremely effective in shielding 3 GHz radiation.

Problem 4.

At the center of L-band (f=1.5 GHz), the min. thickness of fiberglass needed that causes no reflection is

$$d_{min} = \frac{\lambda_2}{2} = \frac{\lambda_{air}}{2\sqrt{\epsilon_r}} = \frac{c/f}{2\sqrt{\epsilon_r}} \approx \frac{3 \times 10^{10} / 1.5 \times 10^9}{2\sqrt{4.6}}$$

$$d_{min} \approx 4.66 \text{ cm}$$

At 1GHz,

$$\lambda_2 = \frac{\lambda_{air}}{\sqrt{\epsilon_r}} \approx 1.0 \text{ cm}$$

Phase constant β follows as

$$\beta_2 = \frac{2\pi}{\lambda_2} \approx 0.449 \text{ rad} - \text{cm}^{-1}$$

Problem 4. Cont.

$$\eta_{23} = \eta_2 \frac{\eta_3 + j\eta_2 \tan(\beta_2 d_{min})}{\eta_2 + j\eta_3 \tan(\beta_2 d_{min})}$$

substituting for $\eta_2 = \frac{377\Omega}{\sqrt{4.6}}$, *and* $\eta_3 = 377\Omega$

$$\eta_{23} \approx 126e^{j36^\circ} \Omega$$

The effective reflection coefficient is

$$\Gamma_{eff} = \frac{\eta_{23} - \eta_1}{\eta_{23} + \eta_1} \approx 0.6e^{j156^\circ}$$

Problem 4. Cont.

Hence the % of the time - average incident power that transmits through the radome at 1GHz can be calculated as

$$\frac{|S_{av}|_t}{|S_{av}|_i} \times 100 = \left(1 - |\Gamma_{eff}|^2\right) \times 100 = 64\%$$

Repeating the same at 2GHz

$$\eta_{23} \approx 126e^{-j36.0} \Omega$$

$$\Gamma_{eff} \approx 0.6e^{-j156^\circ} \Rightarrow \left(1 - |\Gamma_{eff}|^2\right) \times 100 = 64\%$$